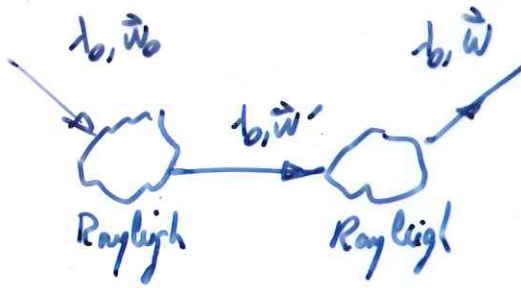


Rayleigh-Rayleigh chain



$$\frac{I}{(R,R)}(\vec{w}, d) = \frac{1 - \sin^2 \gamma}{2} \frac{1 + \sin^2 \gamma_0}{2} \frac{I_0}{17d} \frac{d(1-d_0)}{\frac{\mu_0}{17} + \frac{\mu_0}{17d}} \sigma^2$$

$$\left\{ \int_0^{2\pi} d\varphi' \int_0^1 \frac{dz'}{z'} \frac{[1 + (\vec{w}' \cdot \vec{w}_0^{(+)})^2][1 + (\vec{w}' \cdot \vec{w}_0^{(+)})^2]}{\frac{\mu_0}{17} + \frac{\mu_0}{z'}} \frac{F^2(d_0, \vec{w}', \vec{w}_0^{(+)}, z)}{z} \frac{F^2(d_0, \vec{w}', \vec{w}_0^{(+)}, z)}{z} + \int_0^{2\pi} d\varphi' \int_0^1 \frac{dz'}{z'} \frac{[1 + (\vec{w}' \cdot \vec{w}_0^{(-)})^2][1 + (\vec{w}' \cdot \vec{w}_0^{(-)})^2]}{\frac{\mu_0}{17} + \frac{\mu_0}{z'}} \frac{F^2(d_0, \vec{w}', \vec{w}_0^{(-)}, z)}{z} \frac{F^2(d_0, \vec{w}', \vec{w}_0^{(-)}, z)}{z} \right\}$$

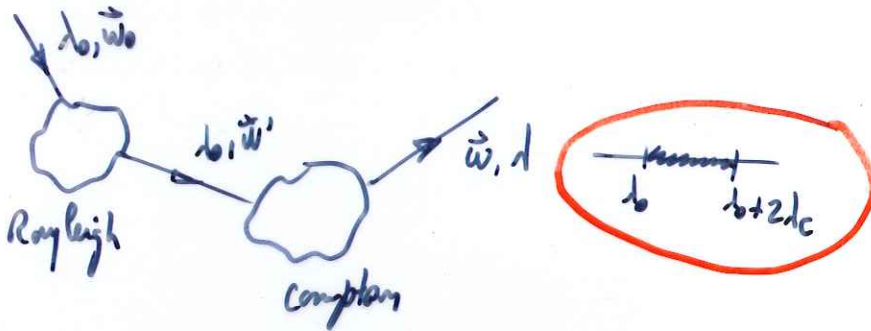
where

$$\vec{w}' \cdot \vec{w}_0^{(+)} = \pm \gamma' \gamma_0 + \sqrt{1 - \gamma'^2} \sqrt{1 - \gamma_0^2} \cos(\varphi' - \varphi_0)$$

$$\vec{w}' \cdot \vec{w}_0^{(-)} = \pm \gamma' \gamma_0 + \sqrt{1 - \gamma'^2} \sqrt{1 - \gamma_0^2} \cos(\varphi' - \varphi_0)$$

- Discrete ($d = d_0$)
- Plane of symmetry
- Modifies also the coherent line

Rayleigh - Compton chain



$$I_{(RC)}^{(2)}(\omega, \lambda) = \frac{1 - \gamma_0^2}{2} \frac{1 + \gamma_0 \gamma_0'}{2} \frac{I_0}{17\lambda_c} \frac{\sigma^2 K_{ev}(\lambda, \lambda_0) S(\lambda_0, a, z)}{\frac{\mu}{17\lambda} + \frac{\mu_0}{17\lambda}}$$

$$\left\{ \int_{\alpha_1}^{\alpha_2} \frac{d\gamma'}{\gamma'} \frac{1}{\frac{\mu_0}{\gamma'} + \frac{\mu}{17\lambda}} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_0^2) - (a-\gamma_0\gamma')^2}} \sum_{i=1}^2 \frac{(1 + (\vec{\omega}_0 \cdot \vec{\omega}'^{(\pm)})^2) F^2(\lambda_0, \vec{\omega}_0, \vec{\omega}'^{(\pm)}, z)}{2} \right\} +$$

$$\left\{ \int_{\beta_1}^{\beta_2} \frac{d\gamma'}{\gamma'} \frac{1}{\frac{\mu_0}{\gamma'} + \frac{\mu}{17\lambda}} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_0^2) - (a+\gamma_0\gamma')^2}} \sum_{i=1}^2 \frac{[1 + (\vec{\omega}_0 \cdot \vec{\omega}'^{(\pm)})^2] F^2(\lambda_0, \vec{\omega}_0, \vec{\omega}'^{(\pm)}, z)}{2} \right\}$$

where

$$a = 1 + \frac{\lambda_0 - \lambda}{\lambda_c}, \quad \varphi_1^{(\pm)} = \varphi + \arccos \frac{a - \gamma_0 \gamma'}{\sqrt{(1-\gamma_0^2)(1-\gamma'^2)}}, \quad \varphi_2^{(\pm)} = \varphi + 2\pi - (\varphi_1^{(\pm)} - \varphi)$$

$$\vec{\omega}_0 \cdot \vec{\omega}'^{(\pm)} = \pm \gamma_0 \gamma' + \sqrt{(1-\gamma_0^2)(1-\gamma'^2)} \cos(\varphi_i^{(\pm)})$$

$$\alpha_1 = \max(0, a\gamma - \sqrt{(1-\gamma_0^2)(1-a^2)})$$

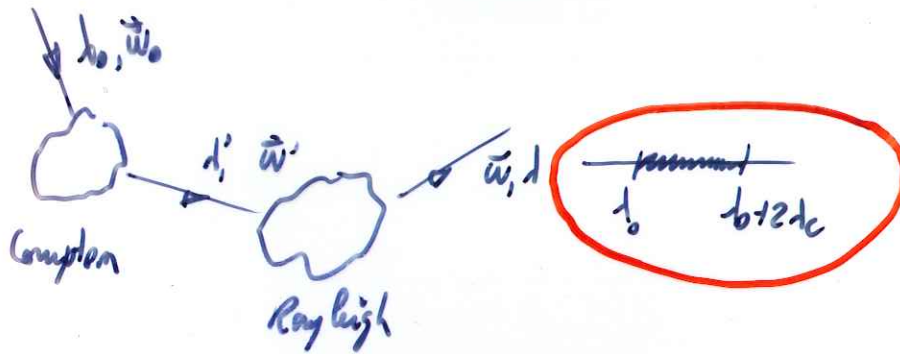
$$\alpha_2 = \min(1, a\gamma + \sqrt{(1-\gamma_0^2)(1-a^2)})$$

$$\beta_1 = -\max(0, a\gamma + \sqrt{(1-\gamma_0^2)(1-a^2)})$$

$$\beta_2 = -\min(-1, a\gamma - \sqrt{(1-\gamma_0^2)(1-a^2)})$$

- Continuous $\lambda \in [\lambda_0, \lambda_0 + 2\lambda_c]$
- Modifies the Compton profile
- Overlaps the Compton-Rayleigh and Compton-Compton spectra
- May overlap other lines

Compton-Rayleigh chain



$$I_{(S,R)}^{(2)}(\vec{w}, \lambda) = \frac{1 - \cos \gamma}{2} \frac{1 + \cos \gamma_0}{2} \frac{I_0}{|\beta_0| \lambda_c} \frac{\sigma^2 K_{WR}(\lambda, \lambda_0) S(\lambda_0, \theta, z)}{\frac{\mu}{|\beta_1|} + \frac{\mu_0}{|\beta_0|}}$$

$$\left\{ \int_{\alpha_1}^{\alpha_2} \frac{d\gamma'}{\gamma'} \frac{1}{\frac{\mu}{|\beta_1|} + \frac{\mu}{\gamma'}} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_0^2) - (a-\gamma'\gamma_0)^2}} \sum_{i=1}^2 \frac{(1 + (\vec{w} \cdot \vec{w}_i^{(i)})^2) F^2(\lambda, \vec{w}, \vec{w}_i^{(i)}, z)}{z} \right\}$$

$$\left\{ \int_{\beta_1}^{\beta_2} \frac{d\gamma'}{\gamma'} \frac{1}{\frac{\mu_0}{|\beta_0|} + \frac{\mu}{\gamma'}} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_0^2) - (a+\gamma'\gamma_0)^2}} \sum_{i=1}^2 \frac{(1 + (\vec{w} \cdot \vec{w}_i^{(i)})^2) F^2(\lambda, \vec{w}, \vec{w}_i^{(i)}, z)}{z} \right\}$$

where $a = 1 + \frac{\lambda_0 - \lambda}{\lambda_c}$, $\varphi_1^{(\pm)} = \arccos \frac{a \pm \gamma' \gamma_0}{\sqrt{(1-\gamma'^2)(1-\gamma_0^2)}}$, $\varphi_2^{(\pm)} = 2\pi - \varphi_1^{(\pm)}$

$$\vec{w} \cdot \vec{w}_i^{(\pm)} = \pm \gamma \gamma' + \sqrt{(1-\gamma'^2)(1-\gamma_0^2)} \cos(\varphi_i^{(\pm)} - \varphi)$$

$$\alpha_1 = \max(0, a\gamma_0 - \sqrt{(1-\gamma_0^2)(1-a^2)})$$

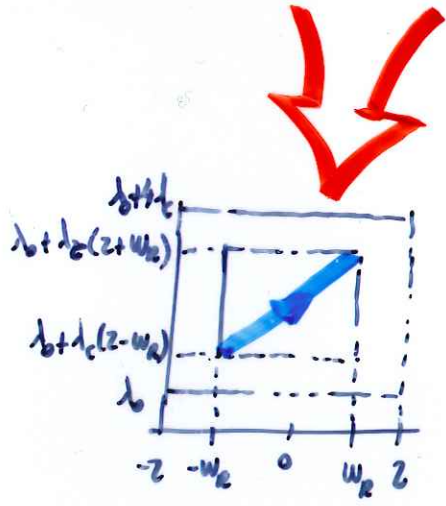
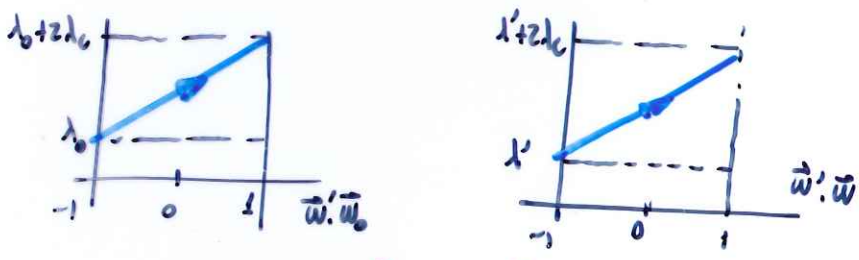
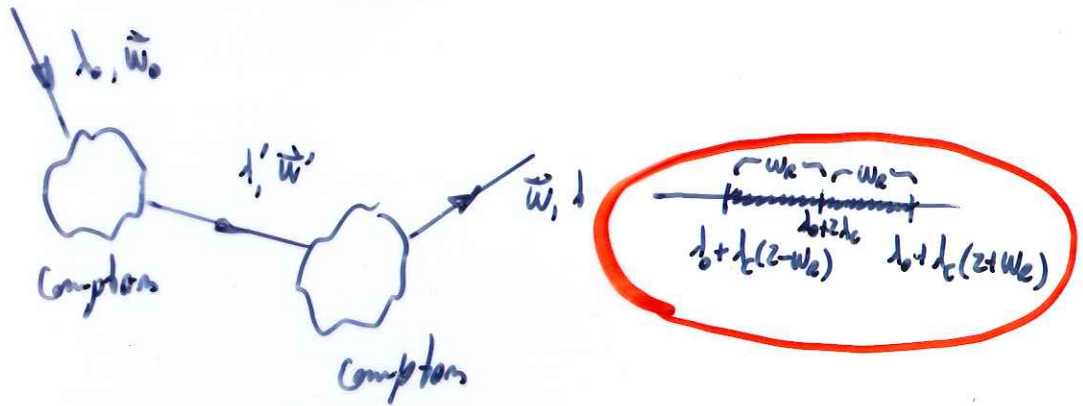
$$\alpha_2 = \min(1, a\gamma_0 + \sqrt{(1-\gamma_0^2)(1-a^2)})$$

$$\beta_1 = \min(0, a\gamma_0 + \sqrt{(1-\gamma_0^2)(1-a^2)})$$

$$\beta_2 = \max(-1, a\gamma_0 - \sqrt{(1-\gamma_0^2)(1-a^2)})$$

- Continuous $\lambda \in [\lambda_0, \lambda_0 + 2\lambda_c]$
- Modifies the Compton profile
- Overlaps the Rayleigh-Compton and Compton-Compton spectra
- May overlap other lines

Compton-Compton chain (detail)



$\vec{w}' \cdot (\vec{w} + \vec{w}_0)$

$\vec{w}_R = \vec{w} + \vec{w}_0$

$w_R = \sqrt{2(1 + \vec{w} \cdot \vec{w}_0)}$

$$I_{(s,c)}^{(2)}(\vec{w}, \lambda) = \frac{1 - \text{sgn } \gamma}{2} \frac{1 - \text{sgn } \gamma_0}{2} \frac{I_0}{|\vec{w}_0|} \frac{\sigma_c}{\frac{\mu}{|\vec{w}|} + \frac{\mu_0}{|\vec{w}_0|}} \int_0^\infty d\lambda' \int \frac{d\vec{w}'}{4\pi} \frac{1}{|\vec{w}'|} K_{KN}(\lambda, \lambda') K_{KN}(\lambda', \lambda_0)$$

$$S(\lambda', \vec{w}, \vec{w}', z) S(\lambda_0, \vec{w}', \vec{w}_0, z) \delta(\lambda_c(1 - \vec{w}' \cdot \vec{w}_0) + \lambda_0 - \lambda') \delta(\lambda_c(1 - \vec{w}' \cdot \vec{w}) + \lambda' - \lambda)$$

$$\left\{ \frac{1 + \text{sgn } \gamma}{2} \frac{1}{\frac{\mu}{|\vec{w}|} + \frac{\mu'}{|\vec{w}'|}} + \frac{1 - \text{sgn } \gamma'}{2} \frac{1}{\frac{\mu}{|\vec{w}_0|} + \frac{\mu'}{|\vec{w}'|}} \right\}$$

Integration over d' and Dirac- δ properties give

$$I_{(S)}^{(2)}(\vec{w}, \lambda) = \frac{1 - \text{sgn} \gamma}{2} \frac{1 + \text{sgn} \gamma_0}{2} \frac{I_0}{|\lambda_0 \lambda_c|} \frac{\sigma^2}{\frac{\mu + \mu_0}{|\lambda|} \frac{\mu}{|\lambda_0|}} \int_{\frac{\pi}{4}} \frac{d\vec{w}'}{|\lambda'|} K_{\text{Ker}}(\lambda, \vec{d}') K_{\text{Ker}}(\vec{d}', \lambda_0)$$

$$S(\vec{d}', \vec{w}, \vec{w}'; z) S(\lambda_0, \vec{w}'; \vec{w}_0, z) \delta\left(z - \vec{w}' \cdot \vec{w}_R + \frac{\lambda_0 - 1}{\lambda_c}\right) \left\{ \frac{1 + \text{sgn} \gamma'}{2} \frac{1}{\frac{\mu + \mu(\vec{d}')}{|\lambda'|}} + \frac{1 - \text{sgn} \gamma'}{2} \frac{1}{\frac{\mu_0 + \mu(\vec{d}')}{|\lambda_0|}} \right\}$$

where $\vec{d}' = \lambda_0 + \lambda_c (1 - \vec{w}' \cdot \vec{w}_0)$

The δ -function can be written as

$$\delta\left(z - \vec{w}' \cdot \vec{w}_R + \frac{\lambda_0 - 1}{\lambda_c}\right) = \delta\left(a - w_R (\gamma' \gamma_R + \sqrt{(1 - \gamma'^2)(1 - \gamma_R^2)} \cos(\varphi' - \varphi_R))\right)$$

where

$$a = z + \frac{\lambda_0 - 1}{\lambda_c}, \quad \gamma_R = \frac{\gamma + \gamma_0}{w_R}, \quad \varphi_R = \arccos\left(\frac{\sqrt{1 - \gamma_0^2} + \sqrt{1 - \gamma^2} \cos \varphi}{\sqrt{w_R^2 - (\gamma_0 + \gamma)^2}}\right)$$

for $w_R \neq 0$ we have

$$\delta\left(z - \vec{w}' \cdot \vec{w}_R + \frac{\lambda_0 - 1}{\lambda_c}\right) = \frac{1}{w_R} \delta\left(\alpha - \gamma' \gamma_R - \sqrt{1 - \gamma'^2} \sqrt{1 - \gamma_R^2} \cos(\varphi' - \varphi_R)\right)$$

where $\alpha = \frac{a}{w_R}$.

The δ -function depends on γ' and φ' . Is it possible to separate it into a part in φ' and a part in γ' ?

The condition into the δ satisfies for some values of $\cos(\varphi' - \varphi_R)$. Since the cosine function is defined in $[-1, 1]$, that condition is equivalent to

$$\frac{(\alpha - \gamma' \gamma_R)^2}{(1 - \gamma'^2)(1 - \gamma_R^2)} \leq 1 \tag{5.4}$$

Condition (C.1) can be written as

$$(\alpha - \gamma' \gamma_R)^2 \leq (1 - \gamma'^2)(1 - \gamma_R^2)$$

or

$$(\alpha^2 + \gamma_R - 1) - 2\alpha\gamma_R\gamma' + \gamma'^2 \leq 0$$

(C.2)

which can be expressed as

$$(\gamma' - \gamma'_1)(\gamma' - \gamma'_2) \leq 0 \quad (\gamma'_1 \text{ and } \gamma'_2 \text{ are the roots of (C.2)})$$

$$\gamma'_{1,2} = \alpha\gamma_R \pm \sqrt{(1 - \gamma_R^2)(1 - \alpha^2)}$$

Then we have that γ' satisfies

$$\frac{\sqrt{(1 - \gamma_R^2)(1 - \alpha^2)}}{\alpha\gamma_R} < \gamma' < \gamma_R$$

We will use also the δ -function property to extract the φ' dependence of the δ

$$\delta[g(x)] = \sum_n \frac{\delta(x - x_n)}{|g'(x_n)|}, \quad g(x_n) = 0, g'(x_n) \neq 0$$

$$\begin{aligned} \delta(\alpha - \gamma' \gamma_R - \sqrt{1 - \gamma'^2} \sqrt{1 - \gamma_R^2} \cos(\varphi' - \varphi_R)) &= \sum_{i=1}^2 \frac{\delta(\varphi' - \varphi'_i)}{|g'(\varphi'_i)|} \\ &= \sum_{i=1}^2 \frac{\delta(\varphi' - \varphi'_i)}{\sqrt{(1 - \gamma'^2)(1 - \gamma_R^2) - (\alpha - \gamma' \gamma_R)^2}} \end{aligned}$$

$$\text{where } \varphi_1 = \varphi_R + \arccos\left(\frac{\alpha - \gamma' \gamma_R}{\sqrt{(1 - \gamma'^2)(1 - \gamma_R^2)}}\right)$$

$$\varphi_2 = 2\pi + \varphi_R - (\varphi_1 - \varphi_R)$$

Finally

$$d(z - \vec{w}' \cdot \vec{w}_R + \frac{d_0 - d}{d_c}) = \frac{1}{w_R} \frac{\delta(\varphi' - \varphi'_1) + \delta(\varphi' - \varphi'_2)}{\sqrt{(1-\gamma'^2)(1-\gamma_R^2)} - (\alpha - \gamma' \gamma_R)^2}$$

$$\left\{ \mathcal{U}(\gamma' - (\alpha \gamma_R - \sqrt{(1-\alpha^2)(1-\gamma_R^2)})) - \mathcal{U}(\gamma' - (\alpha \gamma_R + \sqrt{(1-\alpha^2)(1-\gamma_R^2)})) \right\}$$

By substituting in the last expression of $I_{(SC)}^{(2)}$, we obtain after some algebra

$$I_{(SC)}^{(2)}(\vec{w}, d) = \frac{1 - \text{sgn}(\gamma)}{2} \frac{1 + \text{sgn}(\gamma_0)}{2} \frac{I_0}{|\beta_0| d_c w_R} \frac{\sigma z}{\frac{\mu}{|\beta_1|} + \frac{\mu_0}{|\beta_2|}}$$

$$\left\{ \int_{\alpha_1}^{\alpha_2} \frac{d\gamma'}{\gamma'} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_R^2)} - (\alpha - \gamma' \gamma_R)^2} \sum_{i=1}^2 \frac{K_{\text{KW}}(\lambda_i, \gamma_i^{(+)}) K_{\text{KW}}(\gamma_i^{(+)}, d_0) S(\lambda_i^{(+)}, \vec{w}, \vec{w}_i^{(+)}, z) S(d_0, \vec{w}_0, \vec{w}_i^{(+)}, z)}{\frac{\mu}{|\beta_1|} + \frac{\mu(\lambda_i^{(+)})}{\gamma'}} + \int_{\beta_1}^{\beta_2} \frac{d\gamma'}{\gamma'} \frac{1}{\sqrt{(1-\gamma'^2)(1-\gamma_R^2)} - (\alpha + \gamma' \gamma_R)^2} \sum_{i=1}^2 \frac{K_{\text{KW}}(\lambda_i, \gamma_i^{(-)}) K_{\text{KW}}(\gamma_i^{(-)}, d_0) S(\lambda_i^{(-)}, \vec{w}, \vec{w}_i^{(-)}, z) S(d_0, \vec{w}_0, \vec{w}_i^{(-)}, z)}{\frac{\mu_0}{|\beta_0|} + \frac{\mu(\lambda_i^{(-)})}{|\beta_1|}} \right\}$$

where $\lambda_i^{(\pm)} = d_0 + d_c (1 - \vec{w}' \cdot \vec{w}_0^{(\pm)})$

$$\vec{w}' \cdot \vec{w}_0^{(\pm)} = \pm \gamma' \gamma_0 + \sqrt{1-\gamma'^2} \sqrt{1-\gamma_0^2} \cos(\varphi_i^{(\pm)})$$

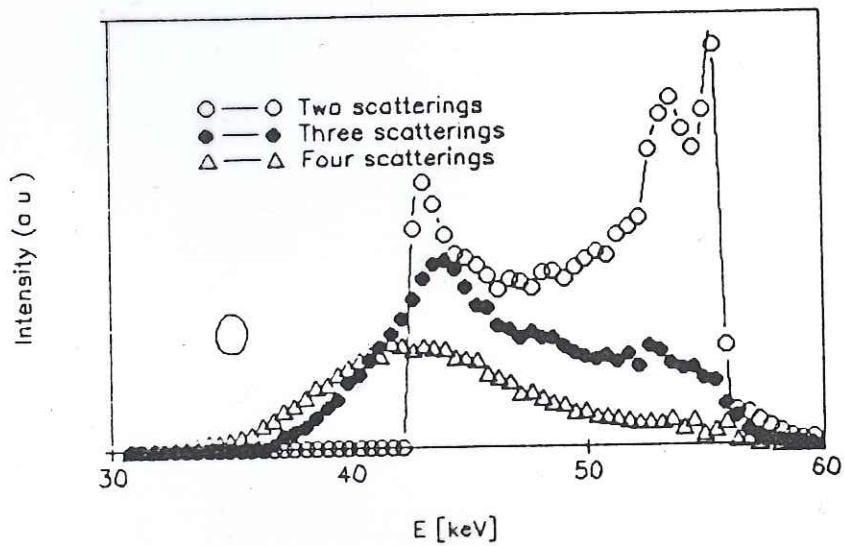
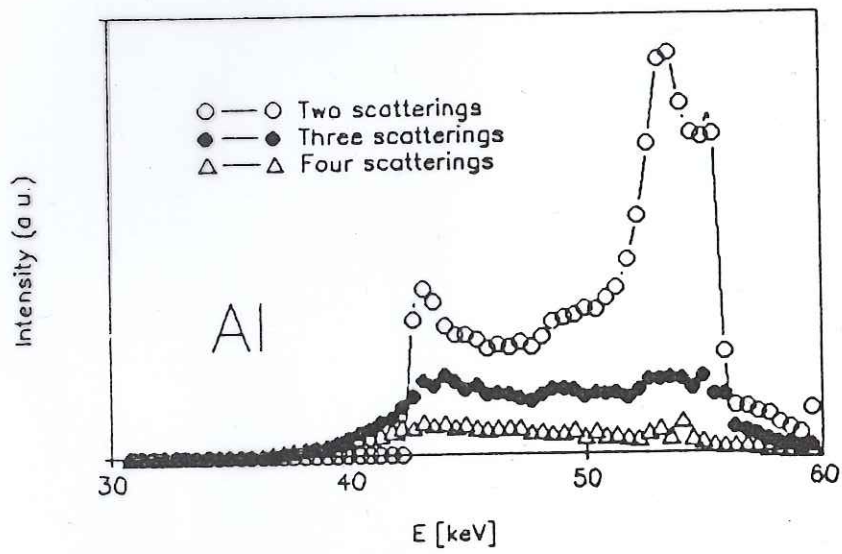
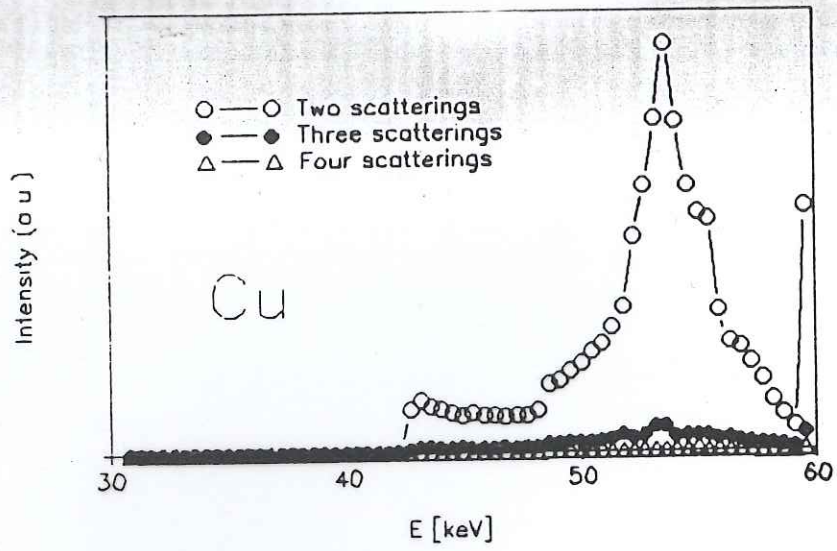
$$\alpha_1 = \max(0, \alpha \gamma_R - \sqrt{(1-\alpha^2)(1-\gamma_R^2)})$$

$$\alpha_2 = \min(1, \alpha \gamma_R + \sqrt{(1-\alpha^2)(1-\gamma_R^2)})$$

$$\beta_1 = -\min(0, \alpha \gamma_R + \sqrt{(1-\alpha^2)(1-\gamma_R^2)})$$

$$\beta_2 = -\max(-1, \alpha \gamma_R - \sqrt{(1-\alpha^2)(1-\gamma_R^2)})$$

- Continuous $d \in [d_0 + d_c (z - w_R), d_0 + d_c (z + w_R)]$
- Overlaps the Compton-Rayleigh and the Rayleigh-Compton claims
- Modifies the Compton profile
- May overlap other lines



Influence of Higher-orders of scattering

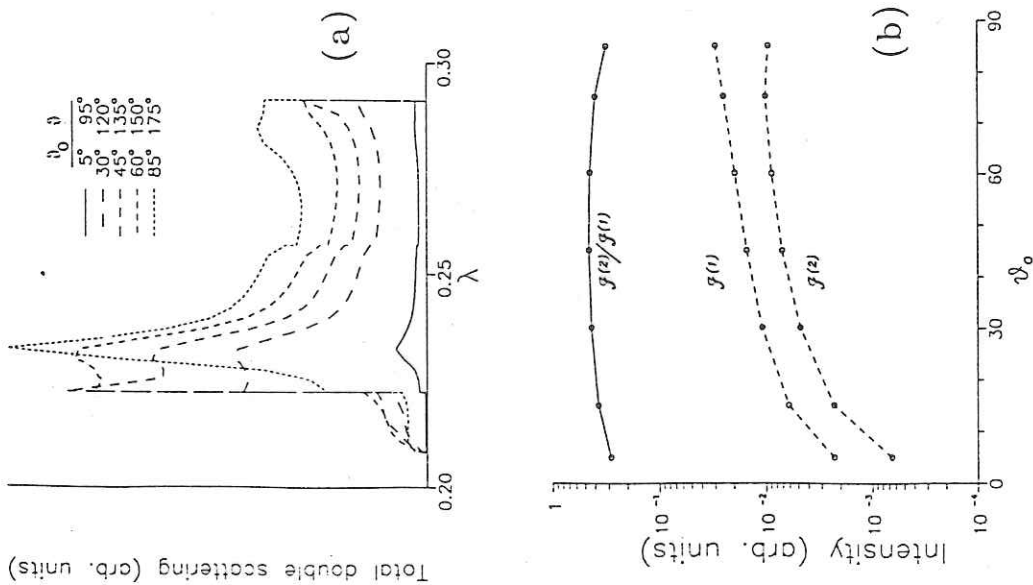


FIG. 7. (a) Double-scattering spectra of Al for a fixed scattering angle of 90° and $E_0 = 59.54$ keV. The incidence (take-off) polar angles are tilted in the scattering plane (maintaining χ unchanged) with values 5° (95°), 30° (120°), 45° (135°), 60° (150°), and 85° (175°), showing the change of the absorption for different geometrical situations. (b) Integrated intensities of single and double scattering as a function of the incidence polar angle for the cases explained above. With a solid line is plotted, in the same graph, the double- to single-intensity ratio which has a maximum near 45° .

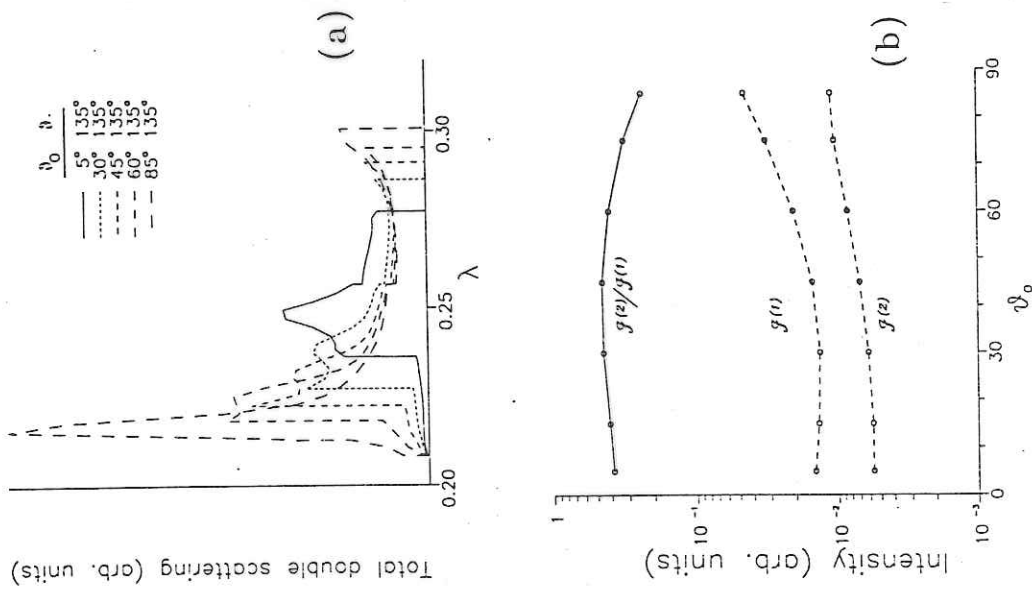


FIG. 8. (a) Total double-scattering spectra of Al, with fixed take-off angle of 135° and $E_0 = 59.54$ keV. The incidence polar angle is tilted in the same scattering plane with values 5° , 30° , 45° , 60° , and 85° . (b) Single and double scattering as a function of the incidence polar angle for Al, with fixed take-off polar angle of 135° and $E_0 = 59.54$ keV. The double- to single-intensity ratio is plotted in the same graph as a solid line.

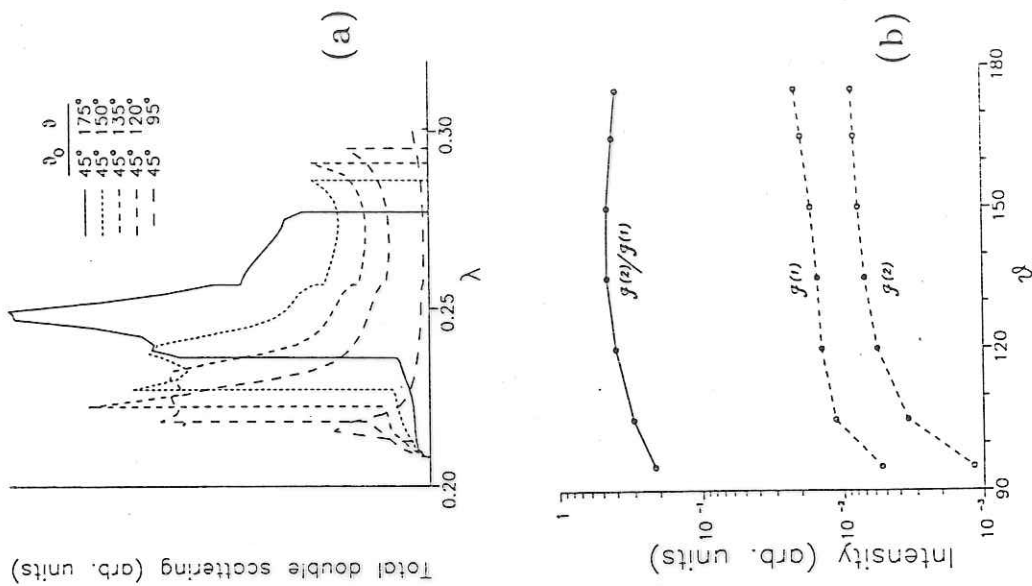
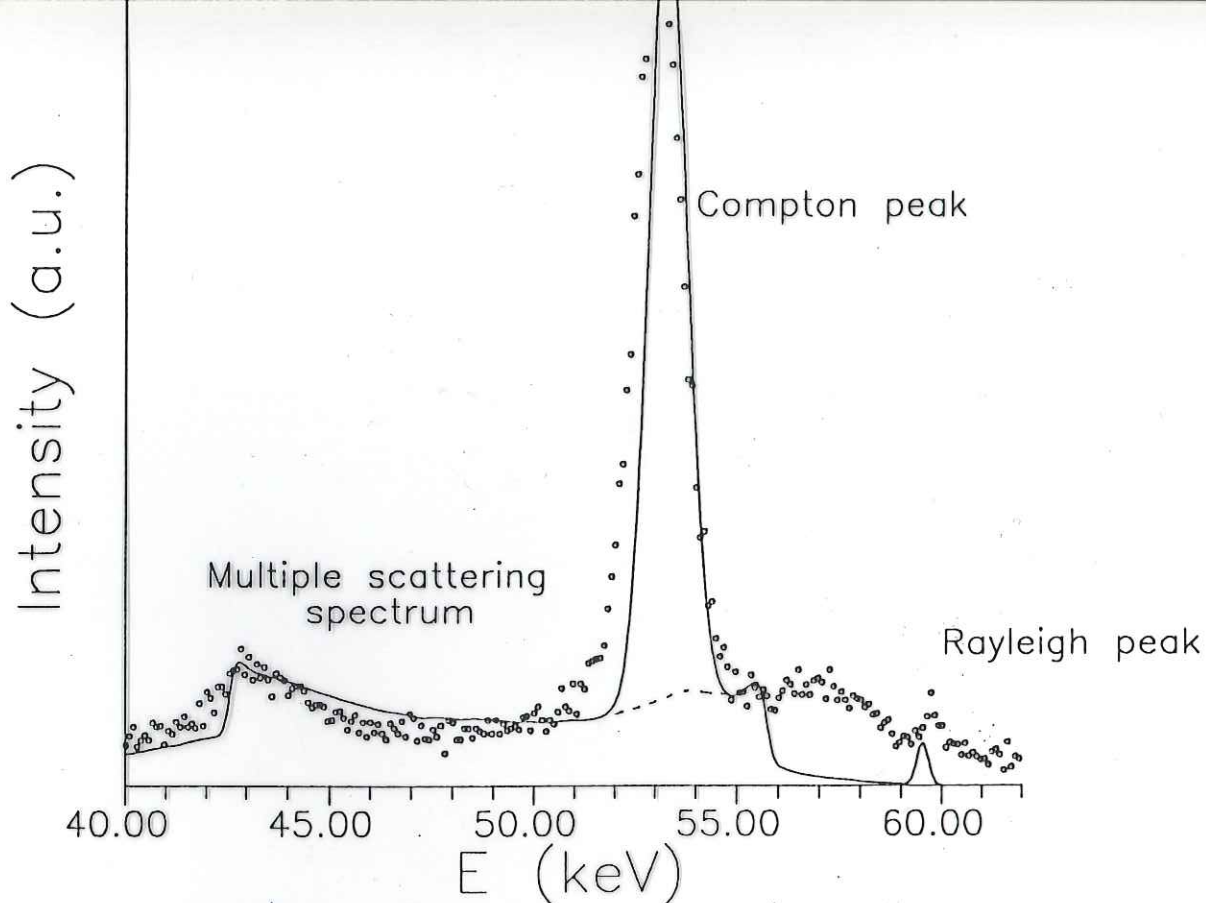
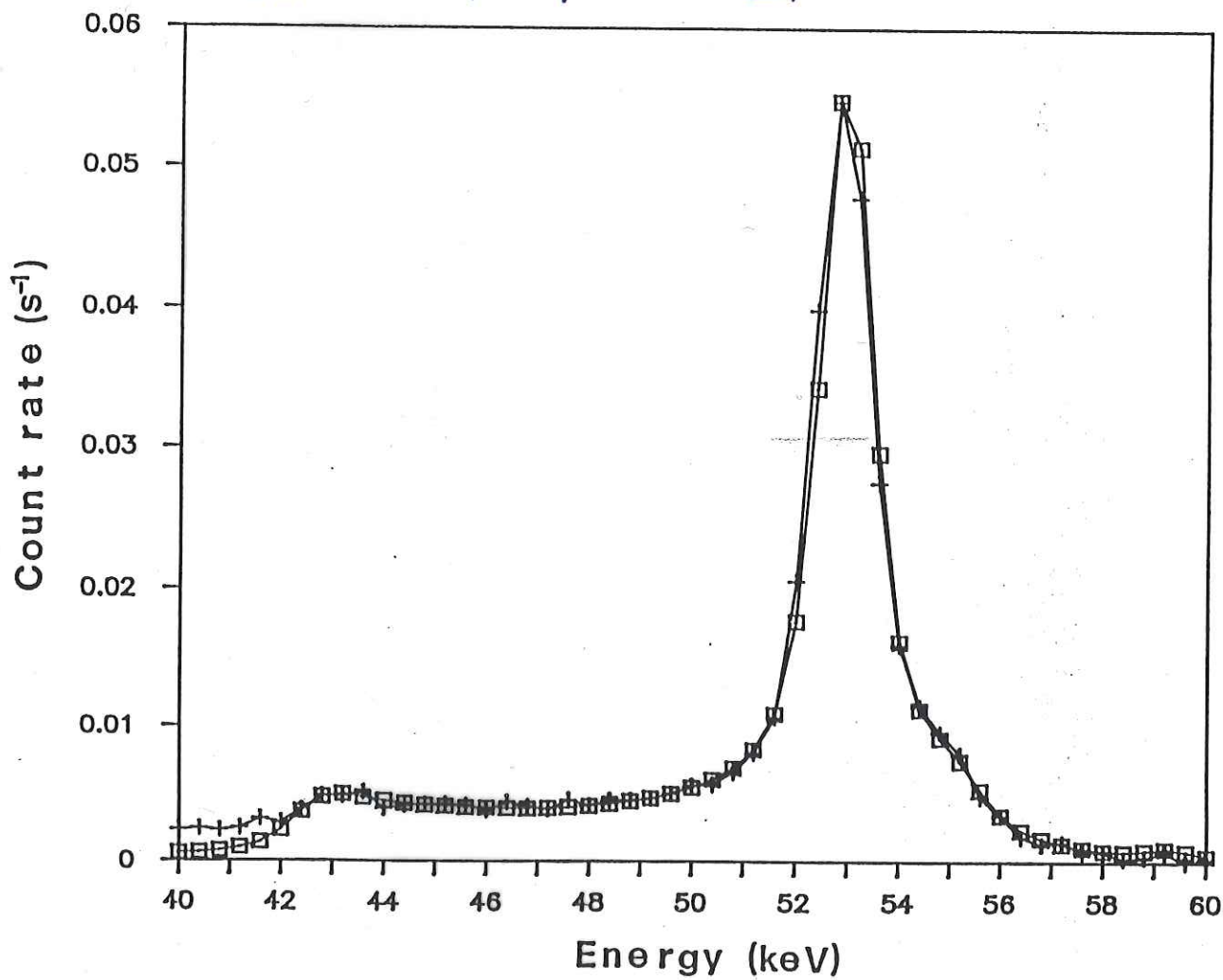


FIG. 9. (a) Total double-scattering spectra of Al, with fixed incidence polar angle of 45° and $E_0 = 59.54$ keV. The take-off polar angle is tilted in the same scattering plane with values 175° , 150° , 135° , 120° , and 95° . (b) Single and double scattering as a function of the take-off polar angle of Al, with fixed incidence polar angle of 45° and $E_0 = 59.54$ keV. The double- to single-intensity ratio is plotted in the same graph as a solid line.



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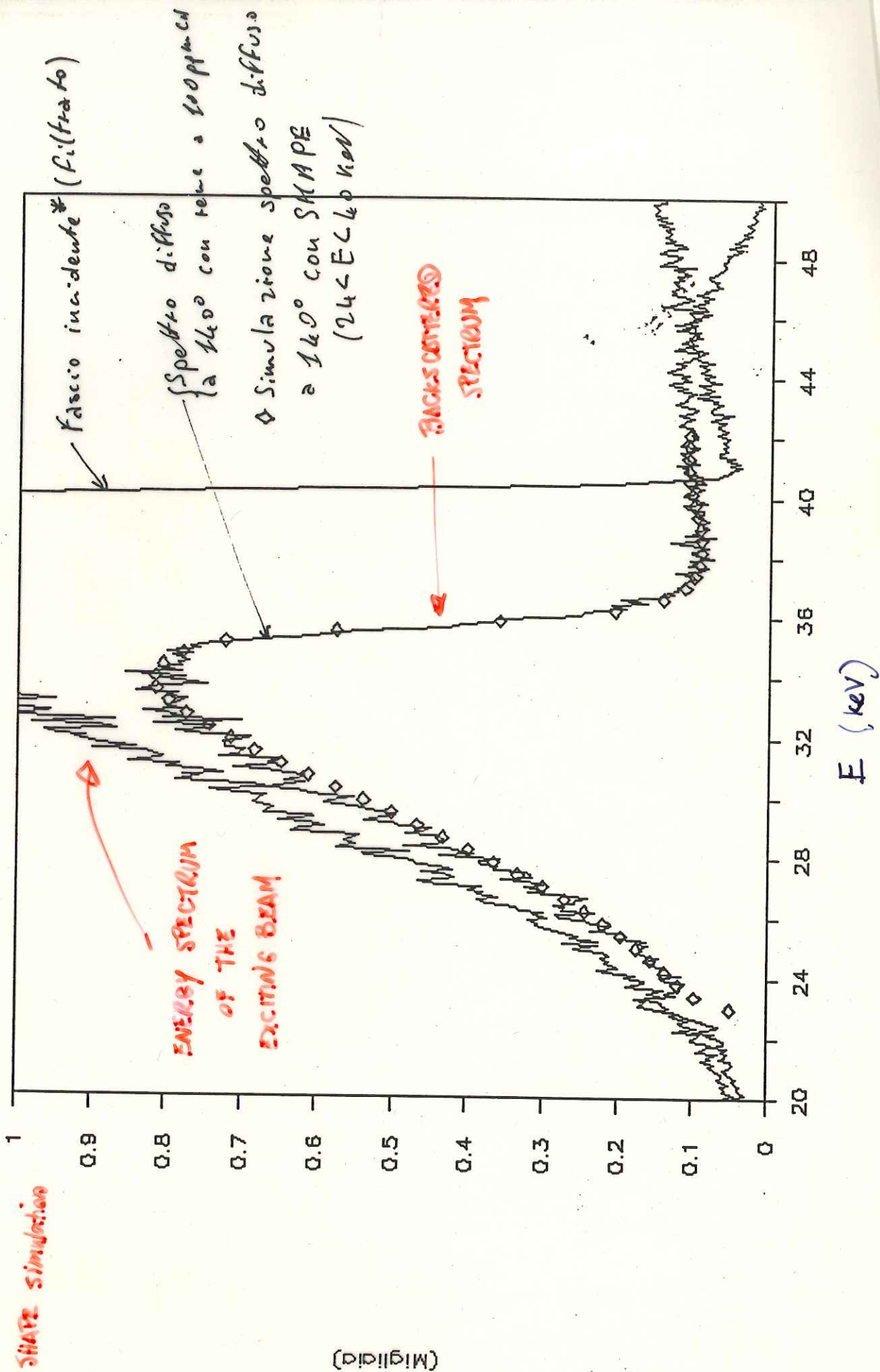
TARTARI et al., X-RAY SPECTROM. 22, 323 (1993)



POLYCHROMATIC EXCITATION ON A BIOLOGICAL TISSUE
 A. TARTARI et al. Phys Med. Biol. 39, 219-230 (1994).

— EXPERIMENTAL

◇ SHAPE SIMULATION



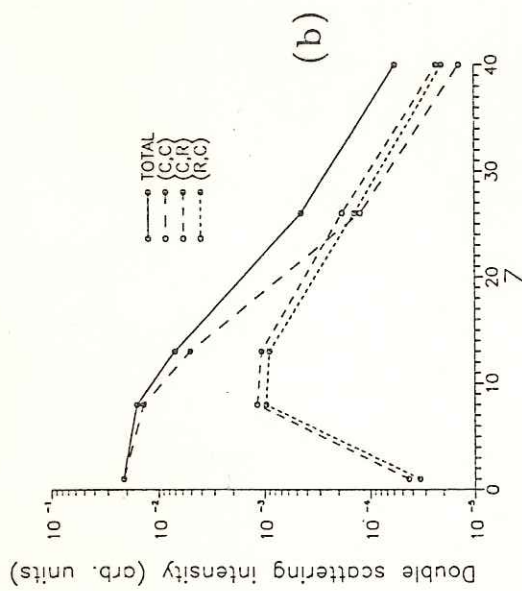
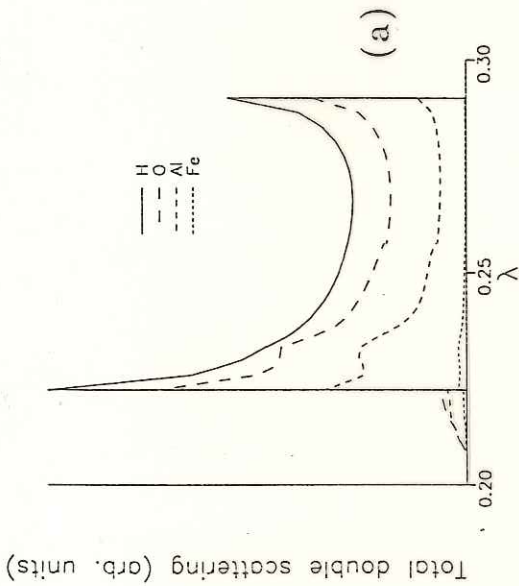


FIG. 5. (a) Total double-scattering wavelength spectra for some elements from H to Fe. The intensity of the double scattering is substantially greater for lighter elements. For heavier elements the Compton-Rayleigh and Rayleigh-Compton mixed contributions become more important. (b) Partial double-scattering intensities as a function of the atomic number Z . The Compton-Compton, Compton-Rayleigh, and Rayleigh-Compton continuous contributions are plotted as a dashed line. The total double scattering is plotted with a solid line. $\vartheta_0 = 45^\circ$, $\vartheta = 135^\circ$, and the energy is 59.54 keV.

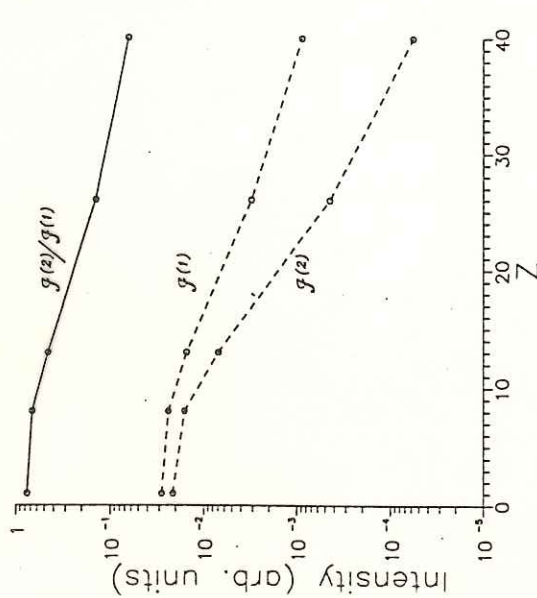


FIG. 4. The single- and double-scattering integrated intensities describing the overall contribution of the corresponding order of scattering. Here they are plotted as a function of the atomic number Z of the target for some representative elements (Li, O, Al, Fe, Zr), polar angles of $\vartheta_0 = 45^\circ$ and $\vartheta = 135^\circ$ and an excitation of 59.54 keV. The double- to single-intensity ratio $g(2)/g(1)$ that gives the importance of the continuous second-order (Compton-Compton, Rayleigh-Compton, and Compton-Rayleigh) terms relative to the intensity of the Compton peak is plotted with a solid line.

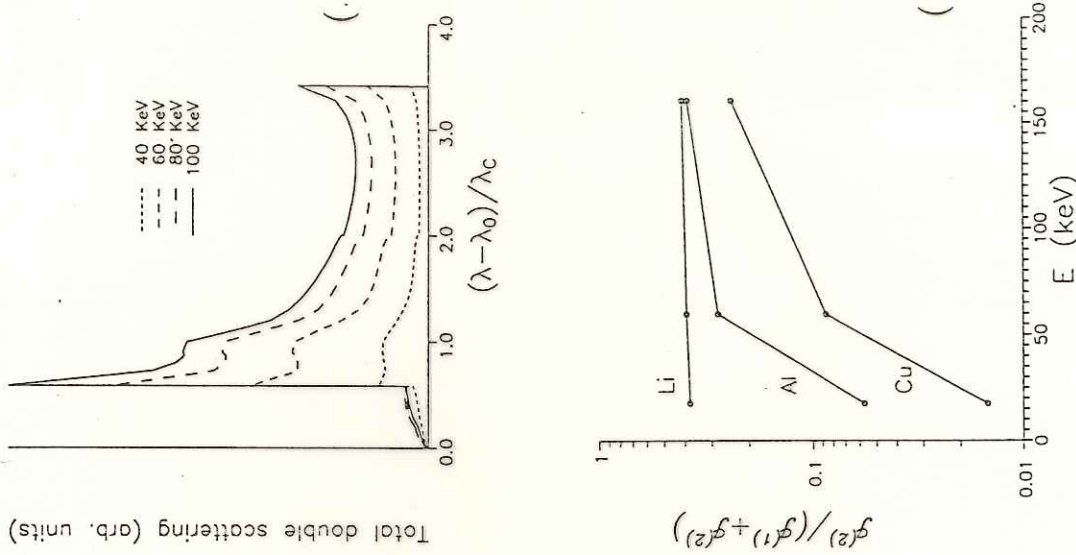
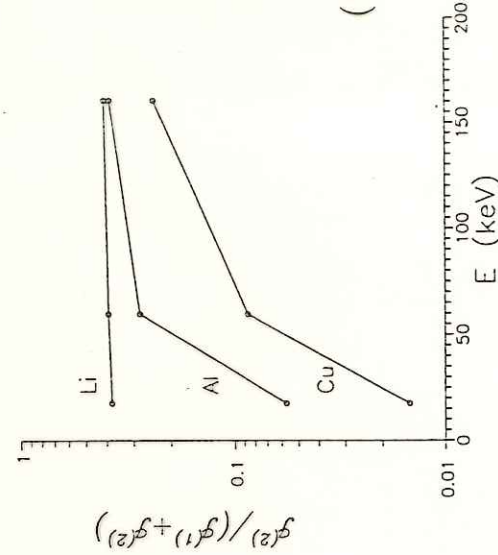
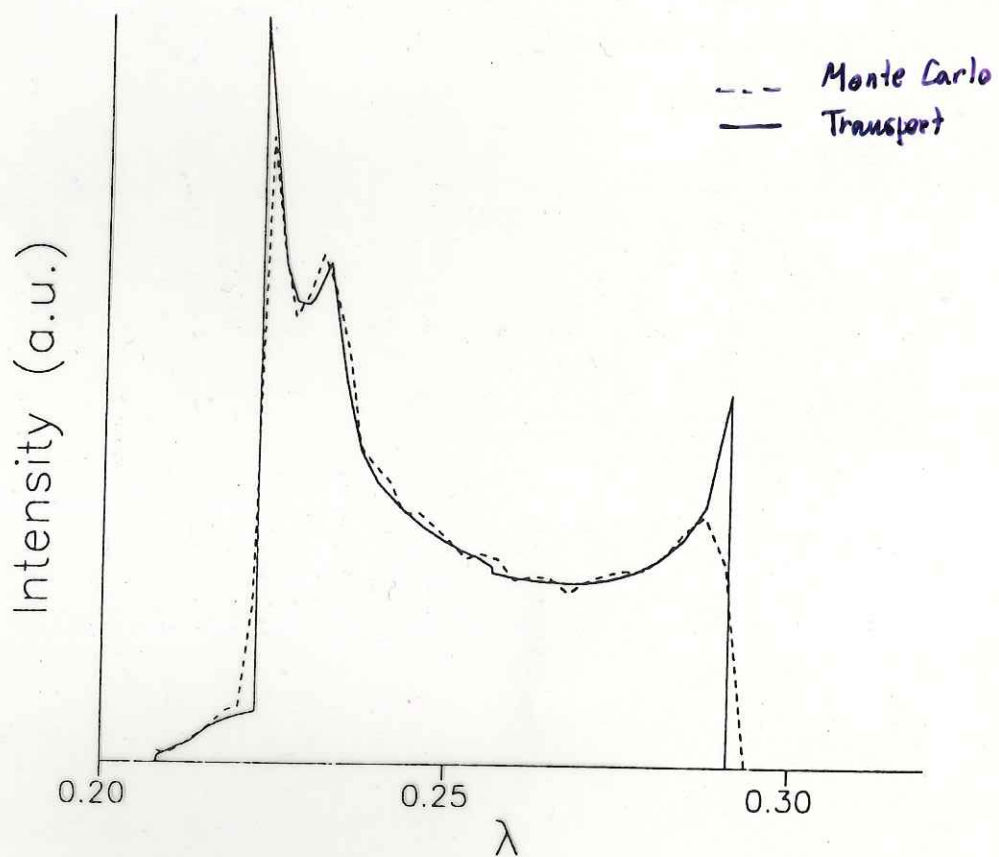
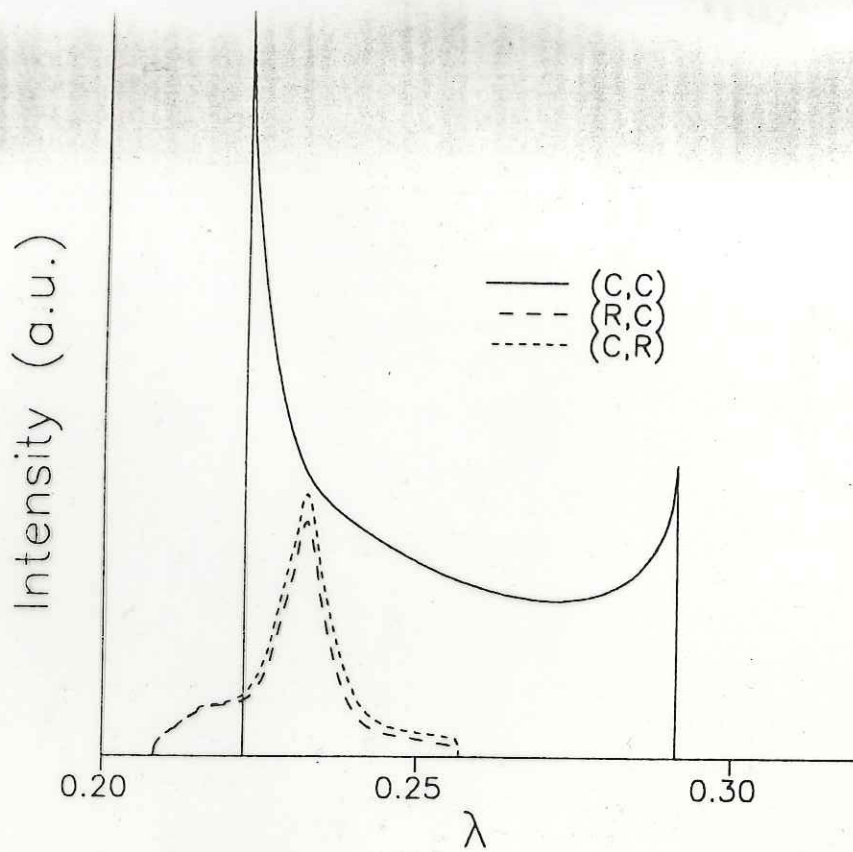


FIG. 6. (a) Total double scattering in Al as a function of the ratio $(\lambda - \lambda_0)/\lambda_c$ for several incidence energies E_0 . The incidence and take-off angles are 45° and 135° , respectively. The double scattering importance β_{double} for Li, Al, and Cu, as a function of the incidence energy E_0 . Three values of E_0 were used in the calculations (17.5, 60, and 160 keV) that approximately correspond to the energy of some excitation lines reported frequently in the literature (Mo $K\alpha$, ^{241}Am and ^{125}Te). The incidence is normal and take-off is 150° . These values may be compared to Monte Carlo simulations performed in similar conditions (Ref. [42]).





Comparison with Monte Carlo (second-order only)